#### Bandwitdh limit and sensitivity of a multimode opto-electomechanical transducer

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### **Outlook**

- 1. About the quantum optics and cryogenic group in Camerino
- 2. Electro-opto mechanics: motivations
- 3. Designing an Electro-opto-mechanics device
- 4. Single mode and multi mode RF-optical transducer
- 5. Proof of principle device and experimental result
- 6. Conclusion and outlook

#### Quantum optics and cryogenic group in Camerino

Theoretical tradition in quantum optics and recently in opto-mechanics (Tombesi, D.Vitali)

Experimental tradition in Cryogenics (superconduction) (R. Natali, "russian school") 1994

Experimental quantum optics activity 2008 (quantum cryptography) (G. Di Giuseppe, R. Natali)

Experimental opto-mechanics (G. Di Giuseppe, R. Natali, D. Vitali) 2010

Experimental electro-opto-mechanics (G. Di Giuseppe, R. Natali, N. Malossi D. Vitali) 2013

Group:

Theory: D.Vitali, F.Zippilli

Experiment: G. Di Giuseppe, R. Natali, N. Malossi, M. Bawai

Projects: HUMOR INFN group 2 ITN-Marie Curie cQOM FP7 iQuoems H2020-FETPROACT: HOT

## Why Electro-opto-mechanics?

Light is optimal for quantum communications between nodes, while microwaves/RF are used for manipulating solid state quantum processors

⇒ a quantum interface between optical and microwave photons would be extremely useful



Quantum interface between optical and microwave photons based on a nanomechanical resonator in a superconducting circuit, simultaneously interacting with the two fields

#### **VARIOUS RECENT EXAMPLES**



#### Piezoelectrically controlled optomechanical crystal

#### **MEMBRANE-OPTICAL-TO-MICROWAVE CONVERTER**



Adding a LC circuit to the membrane-in-the-middle setup, R.W. Andrews et al., Nature Physics 10, 321–326 (2014)

## Electro-opto-mechanics in Camerino: The plan.

1. Realizing an electro-mechanical (High-Q mechanical) device in the RF domain with optical properties.

2. Characterization of the electro-mechanical device by optical and electrical means at room temperature and at cryogenic temperature.

3. Realization of a "RF to optical" transducer at room temperature and cryogenic temperature.

4. Study and developing strategies to increase transducer bandwidth.

5. Realization of a "two-ways RF-optical" transducer, exploiting opto-mechanical interaction (cavity-optomechanics)

6. The asymptotic limit: developing a quantum transducer (cryogenic temperature)

#### **Capacitive coupling: no-contacts capacitor**

High-Q Mechanical Oscillator (SiN 50nm thick) with metal on top



## How do we build a elettro-mechanical oscillator?



Like having two capacitors in series whose capacitance is modulated by the mechanical motion

#### **Coupling with L**

Modulated  $C(x)=C_0+dC(x)$ 



#### Coupling

Designing and building an eletromechanical Oscillator:

/ 1

- 1. Frequency
- 2. Quality Factor

Designing and building an LC Oscillator (Electrical)

- 1. Frequency
- 2. Quality Factor

#### **Designing the eletromechanical oscillator: limits**

## Metalization of the membrane

#### **Restrictions:**

- 1. Optical access
- 2. No contact on the membrane
- 3. Quality factor behavior?
- 4. Decouplig from the frame

Designing of the electrodes

#### **Restrictions:**

- 1. Optical access
- 2. Coupling optimization to the mechanical modes
- 3. Distance from the membrane

#### **Mechanical Mode:**

#### Most important choosing the "best" mechanical mode



 Coupling with light cavity mode: maximal
Eletromechanics: Maximum displacment is exactly where non metal can be placed2.

- 1. Coupling with light cavity mode: hard
- 2. Eletromechanics: Maximum displacment is exactly where metal can be placed.

 Coupling with light cavity mode: good
Eletromechanics: Maximum displacment is exactly where metal can be placed.

#### The metalized membrane:



#### Maximal Area (max coupling)



Minimal Mass (min mode perturbation)

### The mechanical oscillator

Mechanical oscillator: (made by NORCADA) Silicon Nitride membrane: 1mm x1mm, thickness 50nm

Frequency foundamental mode: around 370 kHz (no metal) Quality factor >10^5



## Mechanical oscillator characterization



Noise spectrum:

Standard Interformetry

Shot noise limeted Homodyne Detection

Q factor (Lifetime):

Ring down

#### **Mechanical oscillator properties**

Noise power spectrum: interferometry+homodyne detection



#### **Oscillator quality factor**



Q>100000

#### Problem: identify the modes. Solved by Finite elements Simulation with Comsol





## Modes identification with finite elements simulation



Simulation with 21nm metal layer

#### **Electrode 1**



10x10 mm silicon frame

#### **Electrode 2 «home made electrodes»**



#### Experiment at room temperature.

#### "Sandwich": electro-mechanical device



Did it work? Let's talk about the LC oscillator before

## LC oscillator



Frequency: tunable from 200 khz to Mhz Quality as high as possible

Litz wires and ferrite rods

## Q factor vs frequency



Red -> Room Temperature

Black-> Nitrogen Temperature

#### **Electro-mechanical oscillator**



#### Than... the Hamiltonian (we stay classical)

$$H = \sum_{i} \frac{p_i^2}{2m_i} + \frac{m_i \omega_i^2 x_i^2}{2} + \frac{\phi^2}{2L} + \frac{q^2}{2C(\{x_i\})} - qV$$

#### **RF to Opto Transducer: one mode**



#### **Leading to Langevin Equation**

$$\begin{split} \dot{x}_i &= \frac{p_i}{m_i} \\ \dot{p}_i &= -m_i \omega_i^2 x_i - \frac{q^2}{2} \frac{\partial}{\partial x_i} \left( \frac{1}{C(\{x_i\})} \right) - \gamma_i p_i + F_i \\ \dot{q} &= \frac{\phi}{L} \\ \dot{\phi} &= -\frac{q}{C(x)} - \Gamma_{\rm LC} \phi + V \end{split}$$

- 1) Restricting to one mechanical mode
- linearizing around an equilibrium state by writing each parameter as a sum of a constant + a modulating term (DC+AC terms)

$$\begin{split} \dot{\delta x}_i(t) &= \frac{\delta p_i(t)}{m_i} \\ \delta \dot{p}_i(t) &= -m_i \omega_i^2 \delta x_i(t) - \underbrace{\frac{\bar{q}^2}{2} \frac{\partial^2}{\partial^2 x_i} \left(\frac{1}{C(\{x_i\})}\right)\Big|_{x_i = \bar{x}_i}}_{2m\omega_i \Delta \omega_i} \delta x_i(t) \\ &- \gamma_i \delta p_i - \underbrace{\bar{q}} \frac{\partial}{\partial x_i} \left(\frac{1}{C(\{x_i\})}\right)\Big|_{x_i = \bar{x}_i}}_{G_i} \delta q(t) + F_i \end{split}$$

$$\begin{split} \dot{\delta q}(t) &= \frac{\delta \phi(t)}{L} \\ \delta \dot{\phi}(t) &= -\frac{\delta q(t)}{C(\{\bar{x}_i\})} - \sum_j \underbrace{\bar{q}} \frac{\partial}{\partial x_j} \left( \frac{1}{C(\{x_i\})} \right) \Big|_{x_i = \bar{x}_i}}_{G_j} \delta x_j(t) - \Gamma_{\rm LC} \delta \phi(t) + \delta V(t) \end{split}$$

#### How it looks in the lab...









#### Looking for smoking guns: «static» result

Electrostatic force change equilibrium point and effective spring constant of the mechanical oscillator

$$\Delta\omega_i = \frac{\bar{q}^2}{4m_i\omega_i} \left. \frac{\partial^2}{\partial x_i^2} \left( \frac{1}{C(\{x_i\})} \right) \right|_{x_i = \bar{x}_i}$$

- 1. At first order it is quadratic in Vdc
- 2. It scales with 1/d^3 where d is the distance between the plate.

#### **Mechanical oscillator frequency shift**



Extimating the spacing: d around 30µm (interferometric measurament)

#### Electro-mechanical induced transparency: Resonant case. Single mechanical mode



When the LC-oscillator frequency and the mechanical oscillator frequency are in resonance, the two oscillator interfers destructevely due to the coupling which can be observed in the electrical signal.

#### **Electrical-mechanical Induced transparency:**



LC is driven by an external source and the electrical signal is detected on the plate of the capacitor after decoupling the continuos Voltage, seeded on Network analyzer

G= 240 V/m at Vdc=138V compatible with plates distance around 30 micron

#### **Detecting an RF signal with light**



#### **Optimal transducer: Strong coupling regime**

## Question: How much is the voltage sensitivity of the transducer?



Results from: T.Bagci Nature 507, 81–85

- 1) Close to Strong coupling regime
- 2) d= 1 micron (20 Vdc) (almost the limit)
- 3) Sensitivity 10^9 V/Hz^(-1/2), Bandwitdh 10 khz
  S=10^8 V/(Hz^(-1/2)) 60khz

$$S_{\phi\phi}^{\text{tot}}(\Omega) = (2k)^2 |\chi_{\text{m,eff}}(\Omega)|^2 \left( |G\chi_{LC}(\Omega)|^2 S_{VV}(\Omega) + S_{FF}^{\text{th}}(\Omega) \right)$$
$$S_{VV}^{\text{im}}(\Omega) = \frac{S_{\phi\phi}^{\text{im}}(\Omega)}{|2k\chi_{\text{m,eff}}(\Omega)G\chi_{LC}(\Omega)|^2} = \frac{S_{xx}^{\text{im}}(\Omega)}{|\chi_{\text{m,eff}}(\Omega)G\chi_{LC}(\Omega)|^2}$$

#### **Transducers**



 $S_{\text{out}}(\Omega) = |\alpha_1|^2 |\chi_1(\Omega)|^2 S_{F1}(\Omega) + |\alpha_2|^2 |\chi_2(\Omega)|^2 S_{F2}(\Omega)$  $+ |\alpha_1 G_1 \chi_1(\Omega) + \alpha_2 G_2 \chi_2(\Omega)|^2 |\chi_{LC}(\Omega)|^2 S_{\delta V}(\Omega) + S_{\text{in}}(\Omega).$ 

#### Theory



Costructive interference Increasing bandwitdh between the two modes

Destructive resonance Antiresonance cancellation regime

#### **Degenerate modes**











#### **Experiments: changing G1 and G2 signs**



#### **Dependence over the coupling (Vdc)**



#### Sensitivity and bandwidth



Seeding gaussian RF noise 30 Mhz bandwitdh

#### **Sensitivity and bandwidth**



G1=G2=110 V m<sup>(-1)</sup> (d=30 micron) Faraway from strong coupling regime

Sensitivity 10<sup>(-8)</sup> V/Hz<sup>(1/2)</sup> Bandwitdh around 5 Khz (modes distance)

#### better bandwitdh?



# ... future

#### **1. Testing in cryogenic enviroment... 8 mK**





### 1. Preliminary results indicate 4 micron distance

## 2. Designing supercunducting coils for inductance in cryogenics

#### 2. Going to cavity: RF-opt opt-RF transducer



Membrane in the middle set-up inside in an high finesse optical cavity.





## Conclusions

- 1. We start and set-up an electro-optomechanics experiment in Camerino.
- We investigate the electro-mechanical coupling for different homemade designed oscillator
- We study the increasing of bandwidth detection exploiting constructive interference between multimode mechanical oscillator.

## Thank you